

12 pts

Silicone Blends and Composites for Drug Delivery

BACKGROUND OF THE INVENTION

1. Field of the Invention

5 The present invention relates to implantable medical devices for the controlled, localized delivery of bioactive drugs within a body.

2. Description of the Related Art

10 The systemic administration of drug agents, such as by intravenous means, treats the body as a whole even though the disease to be treated may be localized. Thus, it has become common to treat a variety of medical conditions by introducing an implantable medical device 15 partly or completely into a body cavity such as the esophagus, trachea, colon, biliary tract, urinary tract, vascular system or other location within a human or veterinary patient.

For example, many treatments of the vascular system 20 entail the introduction of a device such as a stent, catheter, balloon, guide wire, cannula or the like. One of the potential drawbacks to conventional drug delivery techniques with the use of these devices being introduced into and manipulated through the vascular 25 system is that blood vessel walls can be disturbed or injured. Clot formation or thrombosis often results at the injured site, causing stenosis (closure) of the blood vessel.

Another cause of stenosis is vascular disease. 30 Probably the most common disease causing stenosis of blood vessels is atherosclerosis. Atherosclerosis is a condition which commonly affects the coronary arteries,

the aorta, the iliofemoral arteries and the carotid arteries.

Many medical devices and therapeutic methods are known for the treatment of atherosclerotic disease. One 5 particular therapy for certain atherosclerotic lesions is percutaneous transluminal coronary revascularization (PTCR), which is a widely performed procedure used to open coronary arteries that have been blocked due to atherosclerotic plaque. PTCR is done most commonly via 10 balloon angioplasty, where a small balloon is threaded into the blocked artery and inflated. Inflation of the balloon "cracks" the atherosclerotic plaque and expands the vessel, thereby relieving the stenosis, at least in part.

15 PTCR is performed more than two million times annually worldwide. While PTCR presently enjoys wide use, it suffers from two major problems. First, the blood vessel may suffer acute occlusion immediately after or within the initial hour after the dilation 20 procedure. Such occlusion is referred to as "abrupt closure." A second major problem encountered in PTCR is the re-narrowing of an artery after an initially successful angioplasty. This re-narrowing is referred to as "restenosis" and typically occurs within the first 25 six months after angioplasty. Restenosis is believed to arise through the proliferation and migration of cellular components from the arterial wall, as well as through geometric changes in the arterial wall referred to as "remodeling."

30 A device such as an intravascular stent including stent grafts and covered stents can be a useful adjunct to PTCR, particularly in the case of either acute or

threatened closure after angioplasty. The stent is placed in the dilated segment of the artery to mechanically prevent abrupt closure and restenosis.

Unfortunately, even when the implantation of the
5 stent is accompanied by aggressive and precise antiplatelet and anticoagulation therapy (typically by systemic administration), the incident of thrombotic vessel closure or other thrombotic complication remains significant, and the prevention of restenosis is not as
10 successful as desired. Restenosis occurs in 30-40% of patients without stents and in 15-30% of patients receiving stents. However, an undesirable side effect of the systemic antiplatelet and anticoagulation therapy is an increased incidence of bleeding complications,
15 most often at the percutaneous entry site.

Other conditions and diseases are also treatable with stents, catheters, cannulae and other devices inserted into the esophagus, trachea, colon, biliary tract, urinary tract and other locations in the body, or
20 with orthopedic devices, implants, or replacements, for example. Unfortunately, bacterial infections are often observed with prosthetic implants and in many cases result in the failure of the devices. Bacteria have a remarkable ability to adhere to surfaces and form
25 biofilms. If they attach to medical implants and cause infection, this phenomenon is referred to as device-associated or biofilm-related infection. Once formed, a biofilm is extremely difficult to eradicate, even with vigorous antibiotic treatments. One object of the
30 present invention is to provide implantable medical devices coated with a layer containing an antibiotic

that would be released in a controlled manner to prevent bacterial colonization and biofilm formation.

One of the drawbacks of conventional means of drug delivery using such coated medical devices is the difficulty in effectively delivering the bioactive agent over a short term (that is, the initial hours and days after insertion of the device) as well as over a long term (the weeks and months after insertion of the device). Another difficulty with the conventional use of stents for drug delivery purposes is providing precise control over the delivery rate of the desired bioactive agents, drug agents or other bioactive material. The term "bioactive agent" is used herein to mean any agent such as a pharmaceutical agent or drug or other material that has a therapeutic effect.

It is desirable to develop devices and methods for reliably delivering suitable amounts of therapeutic agents, drugs or bioactive materials directly into a body portion during or following a medical procedure, so as to treat or prevent such conditions and diseases, for example, to prevent abrupt closure and/or restenosis of a body portion such as a passage, lumen or blood vessel or to prevent bacterial infection.

In view of the potential drawbacks to conventional drug delivery techniques, there exists a need for a device, method and method of manufacture which enable a controlled localized delivery of active agents, drug agents or bioactive material to target locations within a body.

SUMMARY OF THE INVENTION

The foregoing problems are solved and a technical advance is achieved in an illustrative cardiovascular stent or other implantable medical device that provides
5 a controlled release of at least one bioactive agent into the vascular or other system, or other location in the body, into which the stent or medical device is positioned. In one aspect, the present invention provides a composition comprising a blend of silicone
10 elastomer, an adjuvant polymer and a drug for the controlled release of the drug. The composition can be used to form medical devices in part such as a coating or in their entirety. In another aspect, the invention provides for medical devices made in parts or in their
15 entirety from the composition of the invention.

The various features of novelty which characterize the invention are pointed out with particularity in the claims annexed to and forming a part of the disclosure. For a better understanding of the invention, its
20 operating advantages, and specific objects attained by its use, reference should be had to the drawings and descriptive matter illustrated therein and preferred embodiments of the invention set forth below.

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BRIEF DESCRIPTION OF THE DRAWINGS

In the drawings:

Figure 1 is a comparison of release of Paclitaxel from silicone elastomer coatings made with and without 20% PEG into calf serum;

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Figure 2 is a comparison of release of Tranilast from silicone elastomer coatings made with and without 20% PEG into PBS, pH = 7.4;

Figure 3 is a comparison of release into PBS, pH = 7.4 of Tranilast from silicone elastomer coatings with topcoats made of silicone and silicone/PEG;

Figure 4 shows a percentage of methylene blue released;

Figure 5 shows a percentage of methylene blue released-reduced scale;

Figure 6 shows a release rate of methylene blue after one week ($r^2 = 0.88-0.98$);

Figure 7 shows the amount of DENSPM in test disks as a function of disk composition;

Figure 8 shows deformation scores of DENSPM-loaded silicone composites after two weeks soaking in phosphate buffered saline at 37°C, n=3;

Figure 9 shows the Young's modulus (MPa) of DENSPM-loaded films prior to gamma irradiation, as a function of composition, n=3;

Figure 10 shows the Young's modulus (MPa) of DENSPM-loaded films after 2.6MRad gamma irradiation, as a function of composition, n=3;

Figure 11 shows the Young's modulus (MPa) of gamma irradiated, DENSPM-loaded films after two weeks soaking, as a function of composition, n=3; and

Figure 12 shows Kinetic release of DENSPM from PDMS-DENSPM-PEG composites.

DETAILED DESCRIPTION OF THE PRESENTLY PREFERRED EMBODIMENTS

The present invention provides silicone composites (also referred to herein as blends) that are suitable for use as controlled drug delivery as coatings of stents and other implantable devices for example, or as bulk material to form portions or the entirety of implantable medical devices. Hydrophobic molecules can

be delivered directly from silicone composites and the rate of elution modulated by the addition of one or more adjuvant polymers. The initial burst of hydrophilic molecules from the silicone composites is greatly 5 reduced by the presence of the adjuvant polymer and the subsequent release rate can be controlled by the properties of the adjuvant polymer. We have demonstrated that smoother, more uniform composite films can be formed or cast by deposition from solutions prepared 10 from mixtures of solvents and that certain medical devices such as sheaths that are suitable for drug delivery can be formed entirely from these solutions.

Illustrative adjuvant polymers include polyethylene glycol (PEG) having a molecular weight preferably of 15 about 2KDa to 1MDa and most preferably about 2-500KDa, copolymers of ethylene oxide and propylene oxide (EO/PO) such as Pluronic® polymers which exhibit surfactant properties, as exemplified below, as well as any other hydrophilic polymers, including, but not limited to, 20 polysaccharides such as hyaluronic acid and chemically modified cellulose, polyamyloses, polydextroses, dextrans, heparins, heparans, chondroitin sulfate, dermatan sulfate, poly(*N*-isopropylacrylamide), polyurethanes, polyacrylates, polyethyleneimines, 25 polyvinylpyrrolidone, polyvinylalcohol, polyvinylacetate, etc. The therapeutics envisioned for delivery include, but are not limited to: antiproliferatives, anti-inflammatories, antibiotics, antiplatelet agents, anticoagulants, antimicrobials, 30 anti-arrhythmic, antisense therapeutics, and genetic material. The coatings can be used to deliver therapeutics from stents, stent grafts, PICC lines,

catheters, arterial-venous shunts, artery and vein grafts, urological catheters or stents and any other implantable medical devices from which local therapeutic delivery would be beneficial.

5 The present invention further provides implantable medical devices and methods for the controlled, localized delivery of a bioactive agent to targeted locations within a body. The term "controlled localized delivery" as used herein is defined as a characteristic
10 profile release rate of the bioactive agent over a desired period of time at a fixed location. The implantable medical devices of the present invention may have a simple construction, provide a minimal cross-sectional profile, and allow for easy and reproducible
15 loading of active agents, drug agents and bioactive material.

Example 1

Paclitaxel is a lipophilic drug that has been shown
20 to prevent restenosis both with oral administration (Sollott (1995), *J. Clin. Invest.*, **95**: 1869-1876) and local delivery (Axel (1997), *Circulation*, **96**: 636-645, Herdeg (1998), *Semin. Intervent. Cardiol.*, **3**: 197-199, Herdeg (2000), *Z Kardol.*, **89**: 390-397 (abstract), Honda
25 (2001), *Circulation*, **104**: 380-383, Farb (2001), *Circulation*, **104**: 473-479, Drachman (2000), *J. Am. Coll. Cardiol.*, **36**: 2325-2332. Paclitaxel prevents the proliferation of human arterial smooth muscle cells by shifting the balance of microtubule assembly and
30 disassembly towards assembly, thus producing extremely stable unorganized microtubules inside the cytoplasm. Cell replication is thus inhibited in the G₀/G₁ and late

G₂ and/or M phases of the cell cycle Axel (1997) *Circulation*, **96**: 636-645, Schiff (1979), *Nature*, **277**: 665-667). Paclitaxel is a highly lipophilic drug, making it a perfect candidate for local delivery because 5 it can easily pass through the hydrophobic barrier of cell membranes leading to rapid cellular uptake. This property of paclitaxel leads to long-lasting effects, even with small doses.

Tranilast is a hydrophilic drug that has been shown 10 to inhibit migration and proliferation of vascular smooth muscle cells as well as collagen synthesis by these cells (Tamai (1999), *Am Heart J*, **138**: 968-975; Fukuyama (1996), *Can. J. Physiol. Pharmacol.*, **74**: 80-84; Kikuchi (1996), *European Journal of Pharmacology*, **295**: 15 221-227). Several clinical trials have shown that oral administration of Tranilast reduces restenosis rates in patients after PCTA (Tamai (1999) *Am Heart J*, **138**: 968-975, Holmes D (2000) *Am. Heart J*, **139**: 23-31). Local delivery of this drug can allow greater concentration of 20 the drug to reach the artery without increasing systemic plasma levels.

EXPERIMENTAL METHODS:

All samples were dip-coated pieces of 316L 25 stainless steel, measuring 1 cm x 1 cm with 26 gauge thickness. The stainless steel pieces were first cleaned by sonicating in 3% Isopanasol, deionised (DI) water, and acetone, each for 6 minutes, then dipped into the silicone composite solutions of the invention. 30 Silicone elastomer solutions were made with DAP® 100% silicone rubber adhesive (from DAP, Inc., Maryland) co-dissolved with either Paclitaxel or Tranilast and 20 %

(w/w) of polyethylene glycol, MW 3400 (PEG) in methylene chloride. Upon setting, the silicone elastomer solutions formed a film on the steel pieces having a certain thickness. Paclitaxel was loaded at 2% of 5 silicone weight. Tranilast was loaded at 5% of silicone weight. Drug loadings of 100-200 µg/sample were achieved for Paclitaxel and 300-350 µg/sample were achieved for Tranilast. Some samples had a topcoat of silicone elastomer alone. Other samples had a topcoat 10 with PEG to reduce initial burst of drug. All samples were placed in glass culture tubes with 2 mL of either PBS, pH 7.4 or calf serum. The culture tubes were then placed in a shaking water bath at 37°C and 120 rpm. At each time interval, all of the release media was removed 15 and replaced by fresh solution. Paclitaxel samples were assayed using a competitive inhibition enzyme immunoassay (CIEIA) kit from Hawaii Biotech, Aiea, HI. Tranilast samples were assayed using UV spectrophotometry at a wavelength of 340nm.

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RESULTS AND DISCUSSION:

Figure 1 compares the release of Paclitaxel from films deposited on the stainless steel pieces made both with and without 20% weight polyethylene glycol, MW 25 3400. As can be seen in Figure 1, films without PEG have a higher initial burst. Films with PEG, however, have a higher steady state release rate, at 0.38 ± 0.03 µg/day vs. 0.21 ± 0.03 µg/day for films without PEG. Both 30 films exhibit almost zero-order release after the initial burst for the first 60 days, at which point the release rate starts to level off.

Figure 2 compares release of Tranilast from films made both with and without about 20%wt PEG. The films with PEG showed a higher initial release rate, which leveled off to a release rate of zero faster than those 5 without PEG.

To slow the rate of the initial burst and extend the release of Tranilast, topcoats of silicone elastomer and silicone with PEG were added. Topcoats were made with either about 1% or about 10% silicone solutions 10 in a non-polar solvent such as toluene with or without %wt. PEG, resulting in topcoats of various thicknesses. For example, to a solution of 1g silicone and 9g dimethylene chloride (DMC) is added 0.2g PEG. The final concentration of PEG in the topcoat is about 16.7%.

15 Figure 3 compares the release into PBS, pH = 7.4 of Tranilast from silicone elastomer coatings with topcoats made of silicone and silicone/PEG as described above. As can be seen in Figure 3, all of the topcoats reduced the initial burst and lengthened the release time of 20 Tranilast. The silicone topcoat made from the 1% solution without PEG allowed the highest fraction of Tranilast to be released. The silicone elastomer topcoat made from the 10% solution without PEG decreased the initial burst rate the most. In all of these 25 samples, the release leveled off after about 21 days.

For the hydrophobic drug Paclitaxel, the incorporation of PEG into silicone elastomer coatings decreases the initial burst rate and raises the steady state release rate of the drug. Near zero-order release 30 rates were achieved for Paclitaxel after the initial burst for 60 days, with continued but decreased release continuing for as long as 140 days.

For a hydrophilic drug, Tranilast, it was shown that the incorporation of PEG increases the initial burst rate while decreasing the subsequent steady state release rate. Release of the drug was not zero order 5 and leveled off to zero after 21 days. Adding a topcoat to the Tranilast/silicone coating somewhat leveled off the initial burst, but did not extend the release past 21 days.

10 **Example 2**

Comparison of dye release from silicones containing a range of adjuvant polymers

Method: Bulk films were cast into 5cm dia FEP 15 dishes from the solutions using methylene blue as a model drug, RTV 118[®] as the silicone matrix obtained from GE Silicone, of Waterford, NY, and a range PEGs and Pluronic polymers (Ludwigshafen, Germany) as adjuvant polymers. Three molecular weights of PEG were chosen, as 20 were five Pluronic surfactants that varied in molecular weight, physical consistency, and hydrophile-lipophile balance (HLB) (Table 1). Aqueous solutions of adjuvant polymers and methylene blue prepared using a adjuvant polymer:dye mass ratio of 4:1. The solutions were 25 lyophilized and the dry products were ground with a mortar and pestle and sieved to form 180 micron particles. Particles were mixed with 2g of RTV118 in 8g anhydrous toluene by shaking. The established silicone/adjuvant polymer/dye mass ratio of 2.0/0.4/0.1 30 was maintained.

Table 1. Adjuvant polymers used for silicone composites.

	EO content	Physical form	MW Da	HLB
PEG 1.4k	100%	Waxy solid	1450	(Extrapolated to 34.6 from Pluronics data to 100% EO)
PEG 3.4k	100%	Solid	3400	"
PEG 20k	100%	Solid flakes	20000	"
Pluronic 68	80%	Solid granule/powder	8400	29
Pluronic 88	80%	Solid granule/powder	11400	28
Pluronic 127 Prill	70%	Solid granules/	12600	22
Pluronic 127-NR	70%	Solid granule/powder	12600	22
Pluronic 121	10%	Liquid	4400	1

Films were allowed to cure for 3 days. 8mm dia disks were punched from each film, weighed, and soaked in 10ml PBS at 37°C with agitation at 300 rpm. At intervals, samples were transferred to fresh PBS and absorbance at 665 nm was measured.

Results **Figure 4** and **Figure 5** indicate that drug release was faster from PEG compatibilized films than from solid Pluronic compatibilized films, suggesting that the presence of the hydrophobic segment of Pluronic slowed diffusion of the hydrophilic drug. There appeared to be a molecular weight dependence to this effect, with diffusion being slower from matrices containing higher molecular weight Pluronic. Although initial release profiles were similar, extended dye release was greater from high molecular weight PEG than low molecular weight PEG. Differences in PEG particle crystallinity as a function of molecular weight could account for this effect. Biphasic release was observed from the matrix containing the very hydrophobic, liquid Pluronic 121.

adjuvant polymer, suggesting that the diffusion of water into the composite enhanced the diffusion of dye from the material. After one week, the PEG 20k and PL121 materials sustained high release rates. (**Figure 6**). In 5 contrast, the hydrophilic dye burst immediately from the silicone sealant that did not contain hydrophilic adjuvant polymer particles. The burst apparently exceeded the maximum amount of drug calculated to be in the disk. A scan of the dye solution indicated that the 10 peak maxima had not shifted from 665nm, indicating that the dye had not been modified in any way that would result in an artificially enhanced reading. We attribute the discrepancy to non-uniform aggregation of the dye particles within the silicone film in the 15 absence of a stabilizing adjuvant polymer.

Example 3

The present invention also provides a silicone matrix containing PEG-drug particles with low drug 20 burst, sustained drug release, and suitable handling and mechanical properties for wrapping around a vein. Toward this end, we have prepared a series of ~1mm thick sheets from the polydimethylsiloxane (PDMS), polyethylene glycol, and diethylnorspermine (DENSPM). DENSPM is a 25 hydrophilic polyamine drug chosen for its anti-stenotic properties. The compositions used to prepare the sheets are summarized in Table 2 below and illustrated in **Figure 7**. The compositions in the sheets are varied systematically within the following ranges: in PDMS (80- 30 95%wt.), PEG (1-16%wt.) and drug (4-19%wt.).

Table 2:

Sample #	wt% PDMS	wt% PEG	wt% DENSPM	Modulus (MPa)	Modulus (MPa) ^y	Modulus (MPa)*
1	95	1	4	0.6	0.8	0.4
2	90	6	4	1.1	1.43	0.2
3	90	1	9	0.8	1.17	0.2
4	85	11	4	1.9	2.2	0.8
5	85	6	9	3.4	3.5	0.4
6	85	1	14	1.5	2.13	0.5
7	80	16	4	2.6	2.57	1.1
8	80	11	9	3.2	3.23	0.6
9	80	6	14	2.6	3.57	0.5
10	80	1	19	1.7	2.63	0.6

* after γ -radiation

* after γ radiation and 2wk soak

Analysis of the physical characteristics of the sheets
 5 is made to determine the maximum amount of drug and minimum amount of PEG that can be loaded without making films that swell, are too friable, or that release drug too quickly (as would be the case for PEG-free controls) such that a drug-release matrix that approximately
 10 matches the mechanical characteristics of the vein to be sheathed may be obtained. 10 sheets were prepared and kinetic release study was conducted by monitoring the pH's of the 24 h burst phase.

15 **Method:** Samples for Instron testing (4mm working width) and 6 mm dia. disks were cut from the films and sterilized by gamma irradiation (2.6 MRad).

20 **Deformation due to hydration:** Instron samples were soaked in 25ml, 0.2 μ m filter sterilized PBS @ 37°C for two weeks to assess the ability of films to maintain their shape and strength when hydrated. Afterward, the

films were assigned a score from 1-4 based on the degree of deformation as illustrated in **Figure 8**. 1 indicates practically flat and 4 indicates completely curled. The films were desiccated (1atm, room temp, 10-20% relative humidity) for at least three days prior to Instron testing.

Mechanical testing: Instron testing on each of ten compositions with and without gamma irradiation and without soaking. 3 additional gamma irradiated samples from the soaking study described above were tested to determine the effect of hydration and drug release on mechanical properties of the matrices. Film thicknesses were measured with digital calipers and films were stretched at 5cm/min until failure. Modulus, percent elongation at break, and toughness were calculated and compared. For sake of brevity, only modulus is reported in Table 3 and illustrated in **Figure 9** to **Figure 11**.

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Table 3:

Sample #	Deformation Score	Modulus (MPa)	Modulus (MPa) [*]	Modulus (MPa)*
1	2	0.6	0.8	0.4
2	3	1.1	1.43	0.2
3	3.5	0.8	1.17	0.2
4	2	1.9	2.2	0.8
5	3	3.4	3.5	0.4
6	3	1.5	2.13	0.5
7	1	2.6	2.57	1.1
8	1	3.2	3.23	0.6
9	4	2.6	3.57	0.5
10	4	1.7	2.63	0.6

* after γ -radiation* after γ radiation and 2wk soak

Kinetic Release Study. Three disks of each composition and silicone-only controls were placed in 5 ml 0.2 µm filter sterilized PBS (diluted from 10x concentrate) in 20ml scintillation vials. The samples were shaken at 5 300 rpm in a 37°C box. Samples were transferred to fresh PBS aliquots in a laminar flow hood at 1, 2, 4, 10, 14 and 35 day time points. The pH of aliquots from the 1-day time point was measured and the results are discussed below.

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Results:**Deformation due to soaking:**

The results in **Figure 8** indicate that only sample compositions 7 & 8 did not deform. Compositions 10 & 9 15 deformed the most. We think that the high content of hydrophilic PEG & DENSPM contributed to anisotropic swelling of the film. The anisotropy may be due to formation of a thin silicone-rich layer on one side of these films due to settling and depletion of PEG-DENSPM 20 particles from the upper surface during curing. It is interesting that at high hydrophilics content (20%), the increasing amount of DENSPM seemed to contribute to anisotropic swelling. Particles with high DENSPM content (>45%) may be denser and more prone to settling, 25 or may not have sufficient PEG to create the desired interfacial interactions with the PDMS environment to keep the particles well suspended during curing and toluene evaporation.

30 **Mechanical testing:**

There is a slight loss in modulus of the films after gamma irradiation (**Figure 9 & 10**). The modulus of the

soaked and unsoaked materials generally decreased as silicone content increases. This suggests that the particles are having a filling effect and stiffening the matrices. After soaking and desiccation, the modulus of 5 all samples was reduced. The samples that deformed the most (**Figure 8**) had the greatest reduction in modulus, perhaps due to hydration and dissolution of the PEG-DENSPM particles and reduction of the filler effect.

10 **Kinetic release studies.** **Figure 12** shows the kinetic release data of DENSPM in 5 ml PBS at 37 °C for various PDMS-DENSPM-PEG compositions. Compositions 2, 4, 7 and 10 all have relatively low bursts and extended release times. In general, release profile is a strong function 15 of PDMS-DENSPM-PEG composition, with bursts occurring in all compositions with greater than 4% DENSPM, except for composition #10, which has the highest DENSPM content, 19%. Release is observed out to 35 days for compositions 2 & 10.

20 The invention is not limited by the embodiments described above which are presented as examples only but can be modified in various ways within the scope of protection defined by the appended patent claims.

25 Thus, while there have shown and described and pointed out fundamental novel features of the invention as applied to a preferred embodiment thereof, it will be understood that various omissions and substitutions and changes in the form and details of the devices illustrated, and in their operation, may be made by 30 those skilled in the art without departing from the spirit of the invention. For example, it is expressly intended that all combinations of those elements and/or

method steps which perform substantially the same function in substantially the same way to achieve the same results are within the scope of the invention. Moreover, it should be recognized that structures and/or 5 elements and/or method steps shown and/or described in connection with any disclosed form or embodiment of the invention may be incorporated in any other disclosed or described or suggested form or embodiment as a general matter of design choice. It is the intention, 10 therefore, to be limited only as indicated by the scope of the claims appended hereto. All references cited herein are incorporated by reference in their entirety.